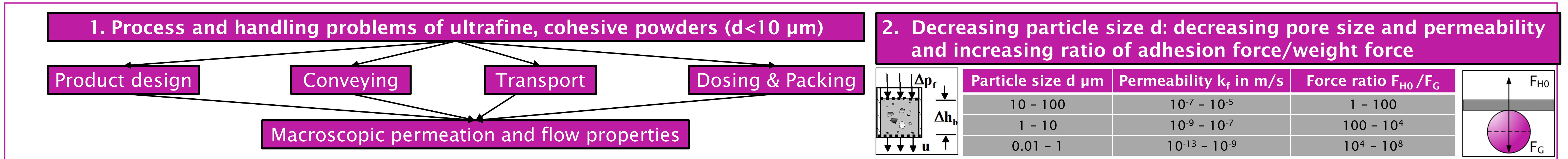


Compression, Consolidation, Permeation & Flow of Ultrafine Cohesive Powders

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Problem Definition

Goal: Understanding of physical **particle** properties at

- Flow-around
 - Approach
 - Contact
 - Detachment
 - Sliding
- Ultrafine, dry and adhesive particles

Objectives

- Combination of Fluid Dynamics (CFD) and Discrete Element Method (DEM) by PFC^{3D} and fluid coupling
- Measurement of macroscopic **powder** properties (compression, consolidation and permeation tests)
- Evaluation of the process (experiments - simulations)

Cooperation

D. Thevenin - U Magdeburg (MD)
Fluid Mechanics, CFD & DEM coupling

A. Kharaghani - U Magdeburg
Pore network and flow simulations

L. Tobiska - U MD:
Numerics of CFD-DEM coupling

S. Luding - U Twente:
Calibration of DEM simulations

K. Mader-Arndt - U MD
Model "Stiff particles with soft contacts"

A. Bertram - U Magdeburg:
Fundamentals of constitutive laws

Flow & Permeation of Powders
Modeling & Simulation

Experimental Methods

1) Compression test and model-based data evaluation

a) Uniaxial powder compression

b) Isentropic compression function

Adiabatic gas compression:

$$\frac{dV}{dp} = \frac{1}{\kappa_{ad} p} \quad (1)$$

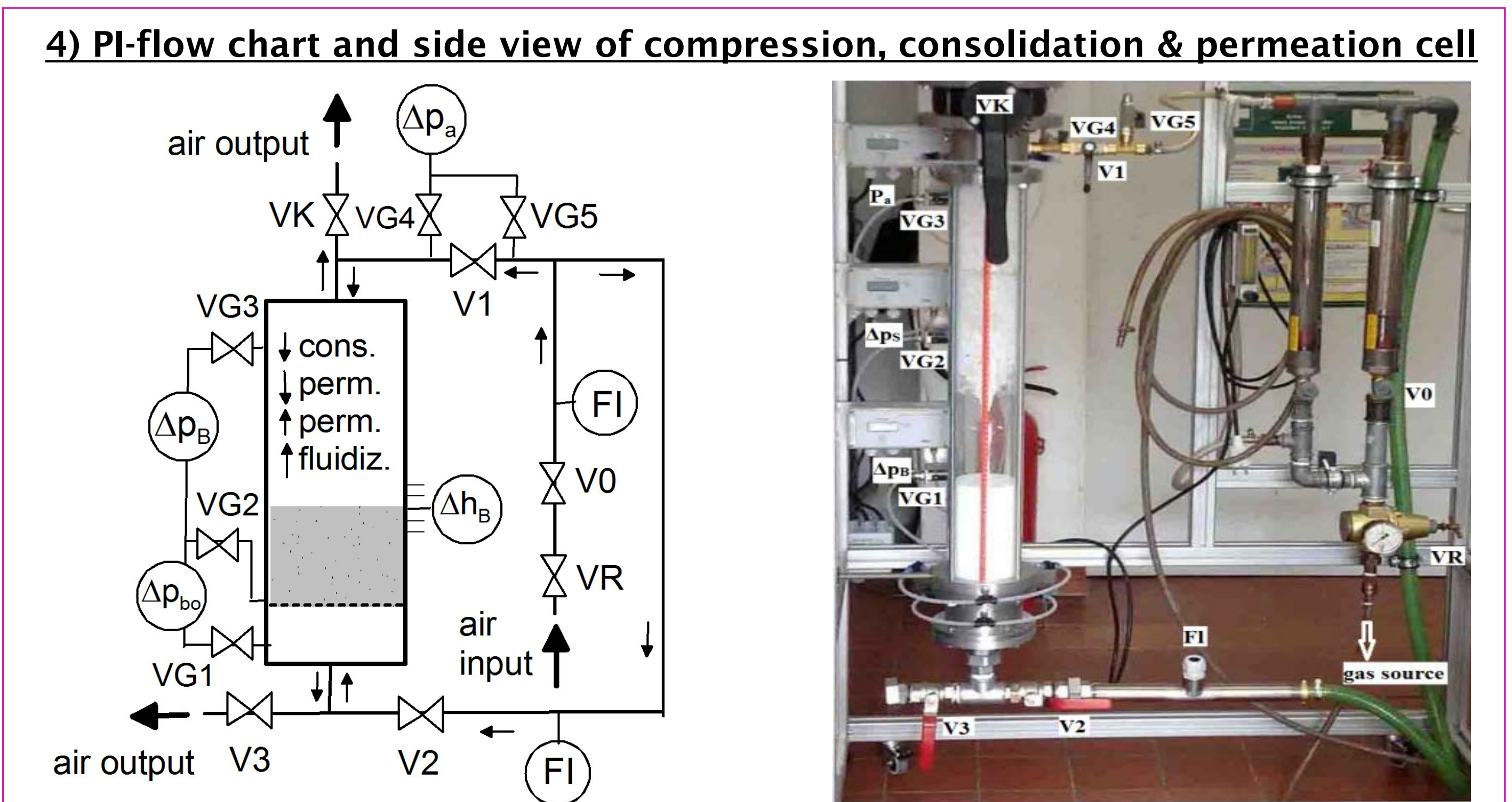
Isentropic powder compression:

$$\int_{\rho_{b,0}}^{\rho_b} \frac{d\rho_b}{\rho_b} = n \cdot \int_0^{\sigma_{M,St}} \frac{d\sigma_{M,St}}{\sigma_{M,St} + \sigma_0} \quad (2)$$

Compressibility index of cohesive powders for small ($1 < \sigma < 50$ kPa) and medium pressures ($50 < \sigma < 1000$ kPa)

Index n	Evaluation	Examples	Flowability
0 - 0.01	incompressible	gravel	free flowing
0.01 - 0.05	low compressibility	fine sand	
0.05 - 0.1	compressible	dry powder	cohesive
0.1 - 1	very compressible	moist powder	very cohesive

New Home-built Test Rig



2) Micro-macro aspects of cohesive powder consolidation and shear

Elastic-Plastic, Frictional Contact:

shear force F_s vs shear displacement s

volumetric strain ϵ_v vs shear displacement s

3) Model-based data evaluation of compression and shear work

mass related preshear and compression work $W_{m,b,pre}$ in J/kg vs centre stress $\sigma_{M,St}$ in kPa

specific power consumption $P_{m,b,pre}$ in mW/kg vs centre stress $\sigma_{M,St}$ in kPa

Data of a very cohesive limestone powder ($d_{50} = 1.2 \mu\text{m}$)

Analytical Description

5) Micro-macro aspects of hindered powder flow

Macroscopic Force Balance at Air Permeated (Counter-flow) Cohesive Powder Bridge:

$$\Sigma F \uparrow = 0 = -F_G + F_r + F_w + F_f$$

Dead weight as driving force:
 $F_G = \rho_p \cdot b \cdot dh_b \cdot g$

Wall force (cohesive resistance):
 $F_w = \sigma_w \cdot \sin \delta \cdot dh_b \cdot \cos \delta \cdot 2l$

Force of inertia:
 $F_r = F_G \cdot \frac{dv}{dt}$

Drag force of air permeation resistance:
 $F_f = Eu_B \cdot \frac{3 \cdot \rho_a \cdot u^2 \cdot (1 - \epsilon)}{4 \cdot d \cdot \epsilon^2} \cdot b \cdot l \cdot dh_b$

Air permeation resistance =

- particle flow-around drag
- macroscopic powder bed resistance (pressure drop)

Macroscopic powder flow resistance in a convergent hopper =

- cohesive flow resistance +
- air permeation resistance

Process Variables	Hopper Discharge and Laminar Permeation through a Cohesive Powder Bridge
Differential equation of motion	$\frac{dv}{dt} + \frac{2(m+1)\tan\theta}{b} \cdot v^2 + \frac{g \cdot B(\epsilon)}{v_{s,St} \cdot \epsilon} \cdot v = g \cdot \left(1 - \frac{b_{min}}{b} - \frac{dp_a/dH}{\rho_b g}\right)$
Permeation resistance acc. to Molerus ¹	$Eu_B = \frac{24}{Re} \cdot \left(1 + 0.692 \cdot \left[\frac{\sqrt[3]{1-\epsilon}}{0.95 - \sqrt[3]{1-\epsilon}} + \frac{1}{2} \cdot \left(\frac{\sqrt[3]{1-\epsilon}}{0.95 - \sqrt[3]{1-\epsilon}}\right)^2\right]\right) = \frac{24}{Re} \cdot B(\epsilon)$
Discharge velocity-time law	$v(t) = \frac{g \cdot \left(1 - \frac{b_{min}}{b} - \frac{dp_a/dH}{\rho_b g}\right) \cdot \tanh\left(\frac{t}{t_{76,lam}}\right)}{\frac{g \cdot B(\epsilon)}{2 \cdot v_{s,St} \cdot \epsilon} \cdot \tanh\left(\frac{t}{t_{76,lam}}\right) + 1}$
Stationary discharge velocity	$v_{st,lam} = \frac{b}{2(m+1)\tan\theta} \cdot \left[\frac{1}{t_{76,lam}} - \frac{g \cdot B(\epsilon)}{2 \cdot v_{s,St} \cdot \epsilon}\right]$
Characteristic discharge (relaxation) time	$t_{76,lam} = \left[\frac{g \cdot B(\epsilon)}{2 \cdot v_{s,St} \cdot \epsilon} + \frac{2g(m+1)\tan\theta}{b} \cdot \left(1 - \frac{b_{min}}{b} - \frac{dp_a/dH}{\rho_b g}\right)\right]^{-1/2}$
Velocity-displacement law	$v_{(t)}(h) = \frac{g \cdot \left(1 - \frac{b_{min}}{b} - \frac{dp_a/dH}{\rho_b g}\right) \cdot \tanh\left(\frac{v_{s,St} \cdot \epsilon}{g \cdot t_{76,lam} \cdot B(\epsilon)} \cdot \left[\frac{4(m+1)\tan\theta}{b} \cdot h + \ln[v_{(t)}]\right]\right)}{2 \cdot v_{s,St} \cdot \epsilon \cdot \tanh\left(\frac{v_{s,St} \cdot \epsilon}{g \cdot t_{76,lam} \cdot B(\epsilon)} \cdot \left[\frac{4(m+1)\tan\theta}{b} \cdot h + \ln[v_{(t)}]\right]\right) + 1} - \frac{1}{t_{76,lam}}$
Differential equation	$\frac{dh(t)}{dt} = \frac{g \cdot \left(1 - \frac{b_{min}}{b} - \frac{dp_a/dH}{\rho_b g}\right) \cdot \tanh\left(\frac{t}{t_{76,lam}}\right)}{\frac{g \cdot B(\epsilon)}{2 \cdot v_{s,St} \cdot \epsilon} \cdot \tanh\left(\frac{t}{t_{76,lam}}\right) + 1} - \frac{1}{t_{76,lam}}$
Displacement-time law	$h(t) = g \cdot t_{76,lam}^2 \cdot \left(1 - \frac{b_{min}}{b} - \frac{dp_a/dH}{\rho_b g}\right) \cdot \left\{\frac{1}{1 - t_{76,lam}^2 b^2} \cdot \ln\left[\tanh\left(\frac{t}{t_{76,lam}}\right) + \frac{1}{t_{76,lam} b'}\right] - \frac{1}{2(1 - t_{76,lam}^2 b^2)} \cdot \ln\left[\tanh\left(\frac{t}{t_{76,lam}}\right) + 1\right] - \frac{1}{2(1 + t_{76,lam}^2 b^2)} \cdot \ln\left[\tanh\left(\frac{t}{t_{76,lam}}\right) - 1\right]\right\}$
Discharge time	Only numerically solvable

¹ Molerus, O., (1993). Principles of Flow in Disperse Systems. Chapman & Hall, London